

1. Description

The μ P6326L5M is a high performance offline AC-DC switcher for mobile phone charger and adapter applications. The device uses Pulse Frequency Modulation (PFM) and Pulse Width Modulation (PWM) multi-mode to build Discontinuous Conduction Mode (DCM) fly back power supplies. The μ P6326L5M uses forward winding for VCC supplies to meet lower standby power, faster startup time and smaller VCC capacitor.

The μ P6326L5M provides accurate Constant Voltage (CV) and Constant Current (CC) without requiring TL431 and opto-coupler. It also eliminates the need of loop compensation circuitry while maintaining stability.

The μ P6326L5M is equipped with both adjustable cable drop compensation function to meet various cables with different lengths and gauges and line voltage compensation function.

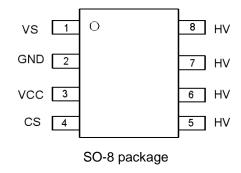
3. Features

- Internal 700V Power BJT for AC Range: 85Vac~264Vac
- Output Power: 15W
- Less than 75mW Standby Power and 1s Startup
 Time
- High Precision Constant Voltage and Current Without TL431 and Opto-coupler
- Multi-mode PWM/PFM Operation for Efficiency and Audio Noise Improving
- Adjustable Cable Compensation (1%~8%)
- Excellent System ESD Performance
- No Need for Control Loop Compensation
- Valley Turn-on to Reduce Switching Loss and Improve EMI
- Operating Frequency Jitter Function for Conductive EMI Suppression
- DoE(VI)/CoC tier2 Compliant Efficiency
- Multiple Protections
 - ◆ Over Temperature Protection(OTP)
 - ◆ Output Over-Voltage Protection(OVP)
 - ◆ Output Short Circuit Protection(SCP)
 - ◆Line Voltage OVP and VCC OVP
 - ♦ VS Resistor Open/Short Protection
 - ◆CS Resistor Open/Short Protection
 - ◆IC Single Pin Floating Protection

2. Applications

- Mobile Phone Charger
- E-tool Adapter
- LED Isolated Power Supply
- Standby Power Supply
- Digital Camera

4. Pin Assignments





5. Pin Descriptions

Pin number	Pin Name	Pin Functions
1	VS	Voltage feedback. The CV and CC regulation are realized based on the voltage sampling of this pin
2	GND	The ground of the IC
3	VCC	The power supply for the IC. In order to get the correct operation of the IC, a capacitor with low ESR should be placed as close as possible to the VCC pin
4	CS	Sense primary side current for turning off the integrated power BJT.
5,6,7,8	HV	The collector pin of the integrated power BJT

6. Absolute Maximum Ratings (Note 1)

Parameter	Name	Range	Unit
Collector voltage of Power BJT	HV	-0.5 to 700	V
Voltage at VCC to Ground	VCC	-0.5 to 38	V
VS input voltage	VS	-30 to 30	V
Voltage at CS to Ground	CS	-0.5 to 6	V
Maximum junction temperature	T _{JMAX}	150	°C
Lead temperature	T _{LEAD}	260	°C
Storage temperature	T _{STG}	-55 to 150	°C
Thermal resistance (Note 2)	θ_{JA}	100	°C/W
Human Body Mode ESD per ANSI/STM5.1-2001		+/-4000	V
Charged Device Model per JEDEC JESD22-C101F		+/-1000	V
Latchup test per JEDEC 78D		+/-200	mA

Note 1: Stresses over those listed under "Absolute maximum ratings" may cause permanent damages to the device. These are stress ratings only. Functional operation beyond those under "Recommended operating conditions" is not implied.

Note 2: The junction-to-ambient thermal resistance under natural convection is obtained in a simulation on a JEDEC-standard, high-K board, as specified in JESD51-7, in an environment described in JESD51-2a

7. Recommended Operating Conditions

Symbol	Parameter	Range	Unit
HV	Power device voltage	0~560	V
VCC	Supply voltage	4~32	V

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8. Electrical Parameter

(Ta=25°C, unless otherwise specified)

Parameter	Symbol	Condition	Min	Тур	Max	Unit
Power supply(VCC pin)						
Quiescent current	Icc	VCC= Vst-1V	280	380	480	μA
Startup voltage	Vst		6	7.5	9	V
Minimum operating voltage	Vuvlo		2.85	3.2	4.5	V
Startup current	lsт	VCC=Vst-1V		0.85	1.5	μΑ
Constant voltage control (VS pin)						
VS regulation voltage	Vvs		-2.91	-2.86	-2.81	V
Cable compensation current at Max load	Ісав	Note 3		50		μΑ
Min. operating frequency	fmin			330		Hz
Constant Current Control (CS pin)						
Threshold voltage @40%~100% Load	Vcsmax		560	590	620	mV
Threshold voltage @0%~5% Load	Vcsmin	Note 3		200		mV
Pre-shutdown voltage	Vcspre/Vcs	Note 3		83		%
Leading edge blanking	TLEB	At Vcsmax		500		ns
Maximum duty of secondary winding conduction	Dмаx	Note 3		0.57		
Frequency jitter						
VCS modulation	ΔVcs/Vcs	Note 3	4	5	6	%
VCS modulation frequency	fмор	Note 3	0.8	1	1.2	kHz
Drive control (Note 3)						•
Drive current	IDRV			84		mA
Overdrive time	Tovd			300		nS
Driving current rising time	T _{DR}	VCC=12V		65		nS
Pull down resistance	Roson			3		Ω
Sinking current rising time	Tsr	VCC=12V		35		nS
Protection function				•		•
Shutdown Temperature	Тотр	Note 3		160		°C
Temperature Hysteresis	Thys	Note 3		25		
VCC overvoltage protection	Vcc_ovp			36.5		V
VS over voltage	Vvs_ovp			4		V
Short circuit voltage	Vvs_HICCUP			0.4		V
Typical time under Vvs(SCP)	tscp	Note 3		64		ms

Note 3: These parameters are guaranteed by design and characterization



9. Functional Block Diagram

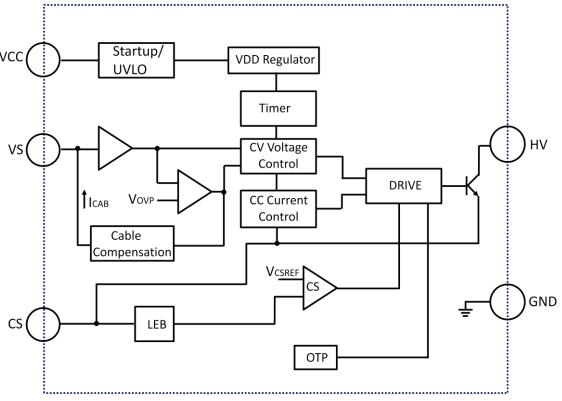


Fig.1, µP6326L5M block diagram

10. Typical Application

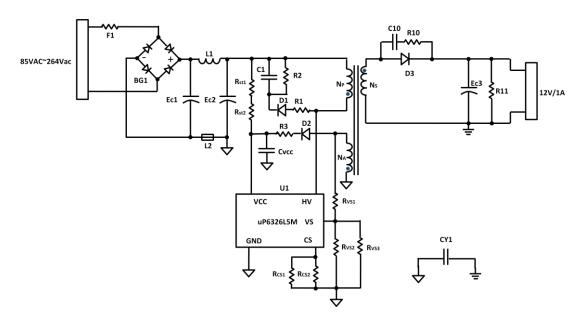


Fig.2, µP6326L5M 12V1A schematic



Ref.	Description	Qty.	Ref.	Description	Qty.
F1	2R 1W	1	Rst1、Rst2	10ΜΩ, 0805, 5%	2
EC1、EC2	10uF/400V, electrolytic	2	R1	100Ω,0805, 5%	1
EC3	470uF/16V, electrolytic	1	R2	200kΩ, 0805, 5%	1
C1	1nF/500V, 0805, ceramic	1	R3	2.4Ω, 0805, 5%	1
Cvcc	470nF/50V, 0805, ceramic	1	Rcs	0.91Ω, 1206, 1%	1
L1	330uH 0510	1	Rvs1	7.5kΩ, 0603,1%	1
L2	10uH 0805	1	Rvs2	6.8kΩ, 0603, 1%	1
CY1	Y1 KX101K	1	Rvs3	62kΩ, 0603, 1%	1
BD1	MBS10 1000V 1A	1	R11	650Ω, 0603, 5%	1
D1	1N4007, SOD-123	1	R12	15kΩ, 0603, 1%	1
D2	IN4148, SOD-123	1	U1	μP6326L5M SOP-8	1
D3	D3 AK5100 DO27		T1	EE16W	1
		Total Con	ponents:26		

Fig.3, µP6326L5M 12V1A BOM

11. Principle of Operation

The typical application circuit of $\mu P6326L5M$ is a conventional flyback converter with a 3-winding transformer---primary winding (N_P), secondary winding (N_S) and auxiliary winding (N_A). The forward auxiliary winding is used for providing VCC supply voltage for IC and sensing the output voltage feedback signal to VS pin.

Fig.4 shows the typical waveforms which demonstrate the basic operating principle of μ P6326L5M application. And the parameters are defined as following.

- I_P---The primary side current
- Is --- The secondary side current
- I_{PK}---Peak value of primary side current
- I_{PKS}---Peak value of secondary side current
- V_{SEC}---The transient voltage at secondary winding
- V_s ---The stable voltage at secondary winding when rectification diode is in conducting status, which equals the sum of output voltage V_O and the forward voltage drop of diode
- V_{AUX}---The transient voltage at auxiliary winding
- V_{A} --- The stable voltage at auxiliary winding when rectification diode is in conducting status, which equals the sum of voltage V_{CC} and the forward voltage drop of auxiliary diode
- t_{sw} ---The period of switching frequency
- t_{ONP} ---The conduction time when primary side switch is "ON"
- t_{ONS} ---The conduction time when secondary side diode is "ON"
- t_{OFF} ---The dead time when neither primary side switch nor secondary side diode is "ON"
- t_{OFFS} --- The time when secondary side diode is "OFF"

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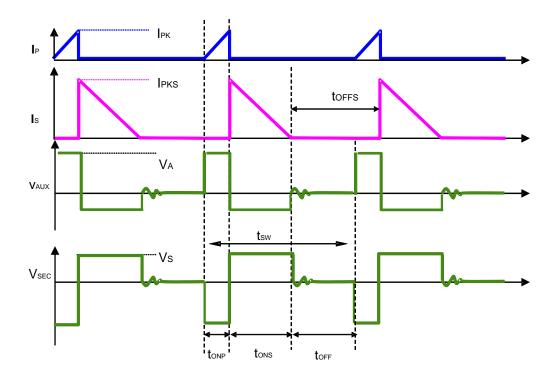


Fig.4 Typical Waveforms

11.1 Proprietary VCC Forward Power Supply

The μ P6326L5M adopts the μ Psemi's proprietary VCC forward power supply technology, which the polarity terminal of auxiliary winding is opposite to the commonly used flyback power supply.

In the traditional VCC flyback power supply, the forward voltage of auxiliary winding is Vo * Nas. The output voltage is very low when starting, Vo * Nas is less than VCC voltage and can't supply VCC power. At this stage the power consumption on VCC is depending on previous storage, so it is necessary to use the large VCC capacitance in order to maintain normal starting.

In the μ Psemi's proprietary VCC forward power supply, as long as the primary side is switched on, the forward voltage of auxiliary winding is 1.414*Vac/Npa and can supply VCC power, which is independent of the output voltage. Therefore, the VCC forward power supply can use smaller VCC capacitor (470nf~1uf generally used), and the starting resistance can be about 20M to achieve lower standby power and faster startup time.

11.2 Constant Voltage (CV) Operation

Constant voltage operation occurs when the load is between no-load and full-load. Output voltage is sensed at the VS pin, which is connected to the auxiliary winding via resistors RVS1 and RVS2. The VS waveform is sampled at tsample , around 2/3 duration of the secondary winding conduction time(Tons). The sampled voltage is regulated at VVS by the voltage control loop. The CV output is determined by the resistors RVS1, RVS2 and the turn ratio of secondary winding to auxiliary winding (Ns/Na). The output voltage at cable end is:



$$V_{O} = |V_{VS}| \times (1 + \frac{R_{VS1}}{R_{VS2}}) \times \frac{N_{S}}{N_{A}}$$

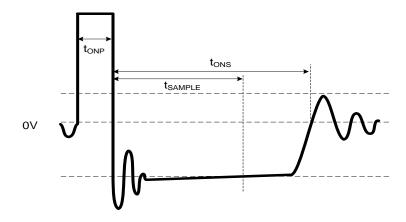


Fig.5 Auxiliary Voltage Waveform

11.3 Adjustable Cable Compensation

The VS pin source a current proportional to load current to generate cable compensation voltage. The cable compensation current at IOMAX is ICAB. The cable compensation voltage VCAB can be adjusted by setting the RVS1, RVS2 values. Neglecting the forward conduction voltage of second D2, the cable compensation voltage at full load is

$$V_{CAB} = I_{CAB} \times R_{VS1} \times \frac{N_S}{N_A}$$

The output voltage at PCB end is

$$V_{OPCB} = V_{O} + V_{CAB}$$

The cable compensation percentage is approximately

$$\frac{V_{CAB}}{V_O} = I_{CAB} \times R_{VS1} // R_{VS2} /|V_{VS}| - 0.05$$

For 5V2A typical application: R_{VS1} =10K Ω , R_{VS2} =13.3K Ω $\frac{V_{CAB}}{V_O}$ =5%

The -0.05 item in the formula is to compensate load regulation.

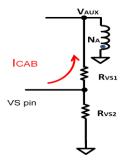


Fig.5. Adjustable Cable Compensation Circuit



11.4 Constant Current (CC) Operation

The μ P6326L5M can work in constant-current (CC) mode. Figure 4 shows the secondary current waveforms. In CC operation mode, the CC control loop of μ P6326L5M will keep a fixed proportion between D1 on-time t_{ONS} and D1 off-time t_{OFFS} . The fixed proportion is

$$\frac{t_{ONS}}{t_{OFFS}} = \frac{4}{3}$$

The relationship between the output current and secondary peak current I_{PKS} is given by:

$$I_{\scriptscriptstyle OUT} = \frac{1}{2} \times I_{\scriptscriptstyle PKS} \times \frac{t_{\scriptscriptstyle ONS}}{t_{\scriptscriptstyle ONS} + t_{\scriptscriptstyle OFFS}}$$

As to tight coupled primary and secondary winding, the secondary peak current is

$$I_{PKS} = \frac{N_P}{N_S} \times I_{PK}$$

Thus the output constant-current is given by:

$$I_{OUT} = \frac{1}{2} \times \frac{N_P}{N_S} \times I_{PK} \times \frac{t_{ONS}}{t_{ONS} + t_{OFFS}} = \frac{2}{7} \times \frac{N_P}{N_S} \times I_{PK}$$

11.5 Switching Frequency Control

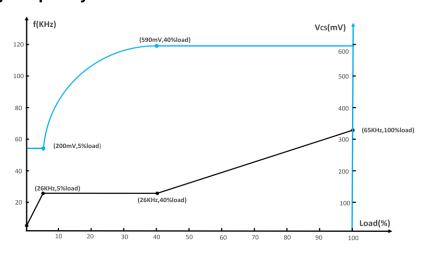


Fig.5, Switching frequency and CS voltage v.s. load current

The µP6326L5M works in Pulse Frequency Modulation (PFM) and Pulse Width Modulation (PWM) multi-mode to control output voltage and current. As shown in Fig.5, the CS voltage at the power device turnoff instant varies from VCSMIN to VCSMAX when the load increases from no load to full load. Operating frequencies varies from 500Hz at no load to up to 65kHz at full load. The power device is turned on when the ring voltage is down to its valley (quasi-resonant switching). This can reduce turn on losses of the power device. It can also generate switching period jittering to reduce EMI.

11.6 Short Circuit Protection (SCP)

Short Circuit Protection (SCP) detection principle is similar to the normal output voltage feedback detection by sensing VS pin voltage. When the detected VS pin voltage is below |VVS_HICCUP |for a duration of about tscp,

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the SCP is triggered. Then the μ P6326L5M enters auto-recovery mode that the IC immediately shuts down and then restarts, so that the VCC voltage changes between V_{ST} and UVLO threshold until V_{VS_HICCUP} condition is removed.

As to the normal system startup, the time duration of VS pin voltage below VVS_HICCUP should be less than t_{SCP} to avoid entering SCP mode. But for the output short condition or the output voltage below a certain level, the SCP mode will be triggered. For typical 5V application, V_{SCP} is about 1V.

$$V_{SCP} = \left| V_{VS_HICCUP} \right| \times (1 + \frac{R_{VS1}}{R_{VS2}}) \times \frac{N_S}{N_A} + I_{CAB} \times R_{VS1} \times \frac{N_S}{N_A} - V_{D2}$$

11.7 Line Voltage OVP

When the Line voltage is over a specified value voltage, power device will be turned off until the line voltage drops below V_{LINE OVP.}

$$V_{LINE_OVP} = 0.707 \times V_{VCC_OVP} \times \frac{N_P}{N_A}$$

11.8 Output Over Voltage Protection

When the output voltage is over a specified value V_{OVP} for 3 successive switching cycles, power device will be turned off until a new startup event begins.

$$V_{OVP} = \left| V_{VS_{-}OVP} \right| \times (1 + \frac{R_{VS1}}{R_{VS2}}) \times \frac{N_S}{N_A} + I_{CAB} \times R_{VS1} \times \frac{N_S}{N_A}$$

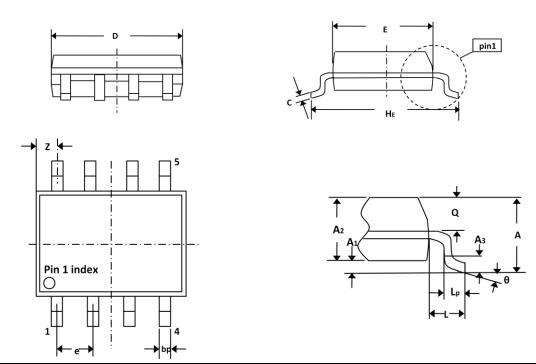


12. Ordering Information

Part number	Mark ID	Package	Packing	Output power		
μP6326L5M	6326L5M	SOP8	4000/Reel	10W~12W		

13. Mechanical dimensions

SOP8



UNIT	Α	A 1	A2	А3	bp	С	D	Е	e	H	L	Lp	Ø	Z	θ
mm	1.75MAX	0.10 0.25	1.25 1.65	0.25	0.31 0.51	0.17 0.25	4.8 5.0	3.8 4.0	1.27	5.8 6.2	1.05	0.4 1.2	0.6 0.7	0.3 0.7	0° 8°